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# SAFETY IMPACTS OF RURAL ROAD CONSTRUCTION







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# SAFETY IMPACTS OF RURAL ROAD CONSTRUCTION

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in cooperation with

Kentucky Transportation Cabinet Commonwealth of Kentucky

and

Federal Highway Administration U.S. Department of Transportation

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### **EXECUTIVE SUMMARY**

Crash data in Kentucky show that the fatal crash rate on two-lane rural roads is substantially higher than on any other type of road. Improvements have been proposed at some locations on this type of road which involve either upgrading the existing two-lane road or adding lanes resulting in a four-lane road. As part of the public information process, highway officials have been asked to document the previous results of this type of construction. The objectives of this study were to: 1) identify sections of two-lane rural roadways where either the two-lane road had been realigned and reconstructed or additional lanes had been added and 2) conduct a before-and-after analysis to determine how these changes affected traffic crashes.

Of the 49 locations included in the study, 25 involved adding lanes and converting to a four-lane road while the two-lane road was upgraded (realignment with wider lanes and shoulders) at 24 locations. Before the construction, the average traffic volume was almost three times higher on the roads where additional lanes were added than where the two-lane road was upgraded. The average daily traffic increased dramatically after the construction was completed with a slightly higher increase for roads where lanes were added.

When all the locations are considered, there was a 51 percent reduction in the crash rate when the road was upgraded and a 56 percent reduction in the crash rate when lanes were added. The rate was reduced from 250 to 122 crashes/100 million vehicle miles (MVM) when the road was upgraded and from 258 to 114 crashes/100 MVM when lanes were added. When only the number of crashes is considered, the number of crashes per mile decreased by 39 percent when the road was upgraded and by 45 percent when lanes were added. The rate of injury or fatal crashes was reduced by 54 percent for upgrading the road and 55 percent by adding lanes while the number of crashes per mile decreased by 43 percent both when the road was upgraded and when lanes were added.

The overall conclusion of the study is that both upgrading two-lane rural roads and converting the road to four lanes are effective methods of reducing total crashes and injury or fatal crashes. The traffic volume would determine the appropriate alternative.

### 1.0 INTRODUCTION

Traffic volumes have increased on all types of roads. On many two-lane rural roads, the combination of the increase in traffic volumes and less than optimum roadway alignment and cross-section have led to increased congestion and crashes. Crash data in Kentucky show that the fatal crash rate on two-lane rural roads is substantially higher than on any other type of road (1). Data for Kentucky for 1995 through 1999 showed a rate of 3.1 fatal crashes per 100 million vehicle miles (100 MVM) for state maintained two-lane rural roads. The next highest rate for any highway type was 1.7 fatal crashes per 100 MVM for four-lane divided (non-interstate and parkway) rural roadways. Also, the total crash rate on four-lane divided (non-interstate and parkway) rural roads was approximately 50 percent lower than for two-lane rural roads (1).

Highway agencies have proposed improvements to some of these two-lane rural roads with the objective of reducing crashes and congestion. The possible improvements typically involve either: a) major revisions to the existing two-lane roadway (usually involving realignment with wider lanes and shoulders and wider clear zones) or b) adding lanes making a four-lane road. However, in some cases, residents have questioned realignments and adding lanes with the argument that the changes may increase traffic volumes and travel speeds and result in more crashes. Highway officials have been asked to document the previous results of these types of construction.

Recent work in this area noted the lack of before-and-after studies documenting the results of conversions of two-lane rural roads to a four-lane roadway (2). Computer models have been used which resulted in estimates of a 40 to 60 percent crash reduction for conversion of a two-lane highway to a four-lane divided highway. Previous research has estimated reduction factors to apply for various types of countermeasures. A 50 percent reduction in crashes was estimated for construction or reconstruction which involved modifying the roadway's horizontal and vertical alignment (3).

The objectives of this study were to: 1) identify sections of two-lane rural roadways where the two-lane road had either been realigned and reconstructed or additional lanes had been constructed resulting in a four-lane road and 2) conduct before-and-after studies to determine the effects of these changes on the number and rate of crashes.

# 2.0 PROCEDURE

The first phase of the study was to identify reconstructed sections of rural highway which could be used in the analysis. Kentucky is divided into 12 highway districts. A survey was sent to each district asking for a list of sections of roadway in their area which could be included as case studies. The information requested included: the location of the construction (county, route, beginning and ending milepoints), the year the construction began and ended, and the number of lanes before and after construction. A statewide list of all major construction projects started since about 1990 was also obtained and used along with the district surveys.

After the surveys were returned, each district was visited and/or contacted to determine specific information about each project. For example, the length of the section was typically changed by a small amount as a result of the construction. Beginning and ending milepoints both before and after construction had to be determined for use in the analysis. The dates the construction started and when traffic started to use the road were also verified. The information from the central file containing all construction projects in the state was used along with information obtained from each district.

Computer records of statewide crash data were available for 1987 through 1999. Therefore, the starting and ending dates of the construction had to fall within certain time periods to allow for the collection of before-and-after data. In most cases, three years of before-and-after crash data were used. Two years were used in several instances with only one year before and after construction used in a very few cases.

Traffic volumes had to be determined to calculate rates. Volume data were obtained from a file which contained volumes for several years. The volume data were defined by county, route, and milepoint. The volume along a section of roadway would generally vary. An average volume for the section was obtained by factoring the volumes and the length of roadway to which it applied.

The before-and-after analysis included a comparison of total crashes, injury and fatal crashes, and other characteristics such as accident type and contributing factors. Crash rates were calculated to determine the change resulting from the reconstruction.

## 3.0 RESULTS

Contacts with the districts resulted in identifying 49 case studies which could be used in the analysis. Data relating to the 49 sections of road at which construction projects were identified are presented in Table 1. The data include the county, route, before-and-after milepoints, construction time period, number of years of before-and-after crash data, and before-and-after traffic volumes.

The sites were divided into the categories of: a) converting a two-lane to a four-lane roadway and b) upgrading the two-lane roadway. Changing to a four-lane road would involve a divided roadway. Upgrading the road would typically involve revising the grade and curvature and providing 12-foot lanes and full-width shoulders and a wider clear zone. Of the 49 locations, 25 involved adding lanes while 24 involved upgrading the two-lane road. The locations were either isolated sections where improvements were made or portions of an larger construction project which extended over a long length of road.

It was necessary to determine, as accurately as possible: a) the dates when construction began and when the road was opened to traffic and b) the start and end locations of each project. In many instances, the beginning and ending milepoints changed slightly after construction. Since

crash data are located using milepoints, accurate milepoint data were necessary. The total length of these sections was about 86 miles where the two-lane road was changed to a four-lane road and about 80 miles where the two-lane road was upgraded. Considering all the locations, the data represent 131 years of before-and-after crash history (as shown by the time period data given in Table 1).

A summary of the total number of crashes before and after the construction is given in Table 2. For each location, the length (specified by the milepoint range), average traffic volume, vehicle miles traveled (100 MVM) over the section, total crashes, and rate (crashes/100 MVM) are given for the before-and-after time periods. The lengths of these time periods are given. The percent change in the crash rate in the after period, compared to the before period, is given. When all the locations are considered, there was a 51 percent reduction in the crash rate when the road was upgraded and a 56 percent reduction in the crash rate when lanes were added. The crash rate was reduced after construction at all but three of the 49 locations. The numbers of crashes were low at these locations. There were a few other locations where the number of crashes was higher after construction but the rate was generally lower after construction so the increase in crashes typically would be related to an increase in traffic volume. There was a small increase in crashes at a few locations which typically only had a very low number of crashes.

The rate was reduced from 250 to 122 crashes/100 MVM when the two-lane road was upgraded and from 258 to 114 crashes/100 MVM when lanes were added. This compares to statewide rates of 252 crashes/100 MVM for two-lane rural roads and 119 crashes/100 MVM for four-lane divided (non-interstate or parkway) rural roads (1). The data show that, before construction, the rates for the two-lane rural roads in this study were very similar to the average statewide rate for that type of road. When the road was changed to a four-lane facility, the overall rate was lowered to a level very close to the statewide rate for this type of road. The rate for the roads which were upgraded, but remained two lanes, was reduced to a level only seven percent above that for the roads which were changed to four lanes which is about one-half the statewide rate for two-lane rural roads.

Before the construction, the average traffic volume was almost three times higher on the roads where additional lanes were added than where the two-lane road was upgraded. The average daily traffic increased dramatically after the construction was completed with a slightly higher increase for roads where lanes were added. The large increase in average daily traffic after the improvements was due to the number of years between the before-and-after volume data. There was usually five to six years between the middle of the before and after time periods. When the number of years between the time periods was considered, the annual increase in traffic volume was about five percent.

The decrease in crash rates was due to a combination of a reduction in number of crashes and an increase in traffic volume. When only the number of crashes is considered, the number of crashes per mile decreased by 39 percent when the road was upgraded and by 45 percent when lanes were added.

The improvements involved both isolated locations and connecting onto longer sections of road where construction had previously been completed. An example of an isolated location is a section of US 119 in Pike County where an approximate three-mile section of two-lane road over a mountain was replaced with a four-lane road. The two-lane road had very sharp curves and steep grades with a large amount of coal truck traffic. The number of crashes in the three years before and after construction was reduced from 72 before to 11 after with the rate reduced 86 percent. An example of extending a four-lane section of road is US 27 south of Nicholasville where almost five miles of road was changed from two to four lanes and connected to the existing four-lane bypass. The number of crashes in the two years before and after construction was reduced from 130 to 85 with the rate reduced 52 percent.

A summary of the total number of injury and fatal crashes before and after construction is given in Table 3. The same types of data are given as for Table 2 with the difference that the crashes involve those in which there was an injury or fatality. When all the locations are considered, there was a 54 percent reduction in the injury/fatal crash rate when the two-lane road was upgraded and a 55 percent reduction in the injury/fatal crash rate when lanes were added.

The percent of crashes involving an injury or fatality changed from 42 percent before to 39 percent after for the upgraded sites and from 36 percent before to 37 percent after for the sites with lanes added. This shows the percentage of crashes involving an injury or fatality did not substantially change as a result of the construction. Considering all data, 34 percent of the crashes involved an injury while 0.9 percent involved a fatality.

There was a decrease of from 19 to 13 fatal crashes at the locations where lanes were added and a decrease of from 4 to 2 fatal crashes at the locations where the road was upgraded. The fatal rate at all locations decreased from 2.23 crashes/100MVM before to 1.16 crashes /100MVM after construction for a decrease of 48 percent.

The injury/fatal rate was reduced from 104 to 48 crashes/100 MVM when the two-lane road was upgraded and from 93 to 42 crashes/100 MVM when lanes were added. This compares to statewide injury/fatal rates of 93 crashes/100 MVM for two-lane rural roads and 44 crashes/100 MVM for four-lane divided (non-interstate or parkway) rural roads (1). The data show that, before construction, the rates for the roads in this study were very similar to the statewide average rate. When the roads were changed to a four-lane facility, the overall rate was lowered to a level very close to the statewide rate for this type of road. When the road was upgraded, this rate was reduced to about one-half the statewide rate for two-lane rural roads.

Injury/fatal crash rates increased at 6 of the 49 locations after the construction. The rate for the roads which were upgraded but remained two lanes was reduced to a level only 14 percent above that for the roads which were changed to four lanes. As previously noted, the decrease in rates was due to a combination of a reduction in number of crashes and an increase in traffic volume. When only the number of crashes is considered, the number of crashes per mile decreased by 43 percent both when the road was upgraded and when lanes were added.

An analysis of the characteristics of the crashes is presented in Table 4. Data concerning the type of crash, directional analysis (which is a more detailed description the type of crash), light condition, road surface condition, human contributing factors, and environmental contributing factors are given. The most common type of crash involved a collision with another motor vehicle with the rates decreasing for all types of crashes. The distribution of the crashes by general type of crash did not change substantially. While the rates for crashes at intersections decreased after the construction projects, the percentage of crashes which occurred at an intersection increased due primarily to the increase in the percentage of angle collisions.

The decrease in the rate of crashes during darkness was similar with that for all crashes with a larger decrease in the rate when the road surface was wet or snow covered. The rate and percentage of crashes involving unsafe speed decreased dramatically. This contradicts the theory that the improved roadway geometrics would result in higher speeds which would then cause crashes. While speeds would logically increase on the new roads, the design of the road would allow for the road to be driven safely at higher speeds. The percentage of crashes in which a driver failed to yield the right of way increased when lanes were added. Considering all the types of factors included in the environmental area, the percentage of crashes involving an environmental factor decreased (due primarily to a decrease in crashes involving a slippery surface) but crashes involving an animal action (primarily deer collisions) increased.

# 4.0 CONCLUSIONS

The comparisons of crash data before and after reconstruction of two-lane rural roadways showed that a substantial reduction in the number and rate of crashes resulted from the construction. When all the locations are considered, there was a 51 percent reduction in the crash rate when the two-lane road was upgraded (realignment with wider lanes and shoulders and a wider clear zone) and a 56 percent reduction in the crash rate when the two-lane road was converted to four lanes. The rate was reduced from 250 to 122 crashes/100 MVM when the two-lane road was upgraded and from 258 to 114 crashes/100 MVM when lanes were added. When only the number of crashes was considered, the number of crashes per mile decreased by 39 percent when the road was upgraded and by 45 percent when lanes were added. The rate of injury or fatal crashes was reduced by 54 percent when upgrading the road and 55 percent when adding lanes with the number of crashes per mile decreased by 43 percent both when the road was upgraded and when lanes were added.

The overall conclusion of the study is that both: a) upgrading two-lane rural roads through realignment and wider lanes, shoulders, and clear zones and b) converting the road to four lanes are effective methods of reducing the number and rate of total crashes as well as injury or fatal crashes. The traffic volume would determine the appropriate alternative with four lanes necessary as traffic volumes increase. Before the construction at the case study locations, the average traffic volume was almost three times higher on the roads where additional lanes were added than where the two-lane road was upgraded.

# **5.0 REFERENCES**

- 1. Agent, K.R. and Pigman, J.G.; "Analysis of Traffic Accident Data in Kentucky (1995-1999)," Kentucky Transportation Center, University of Kentucky, KTC-00-17, September 2000.
- 2. Council, F.M. and Stewart, J.R.; "Safety Effects of the Conversion of Rural Two-Lane to Four-Lane Roadways Based on Cross-Sectional Models," Transportation Research Board Record 1665, October 1999.
- 3. Agent, K.R.; Stamatiadis, N.; and Jones, S.; "Development of Accident Reduction Factors," University of Kentucky, KTC-96-13, June 1996.

**Table 1. Summary of Highway Construction Locations** 

|                 |                     |                        |               |                        |                  | Average        |              |
|-----------------|---------------------|------------------------|---------------|------------------------|------------------|----------------|--------------|
| Country         | Dauta               | Milepoint Ra<br>Before | nge<br>After  | Construction<br>Period | Time Before/     | Traf<br>Before | fic<br>After |
| County          | Route               | Delore                 | Arter         | Period                 | After Data (Yrs) | Бегоге         | Arter        |
| Converting from | om two to four lane | es                     |               |                        |                  |                |              |
| Anderson        | US 127 B            | 0.0-6.831              | 0.0-6.656     | 1990-1992              | 3                | 8,838          | 14,041       |
| Anderson        | US 127              | 9.161-11.789           | 8.9-11.12     | 1990-1992              | 3                | 6,410          | 5,790        |
| Bell            | US 25 E             | 14.481-19.473          | 14.481-18.711 | 1992-1995              | 3                | 7,540          | 9,500        |
| Boyle           | US 127              | 0.0-2.972              | 0.314-3.443   | 1992-1994              | 3                | 9,369          | 12,546       |
| Bullitt         | US 31 E             | 3.2-5.465              | 3.2-5.185     | 1992-1996              | 3                | 10,200         | 13,580       |
| Christian       | US 68               | 7.3-8.75               | 7.3-8.75      | 1995-1997              | 2                | 5,900          | 6,900        |
| Daviess         | US 60               | 19.332-23.558          | 19.326-23.842 | 1994-1997              | 2                | 10,219         | 15,539       |
| Floyd           | US 23               | 21.297-23.801          | 20.445-21.878 | 1991-1994              | 3                | 10,200         | 12,600       |
| Floyd           | US 23               | 18.153-21.296          | 17.489-20.444 | 1991-1993              | 3                | 14,500         | 15,700       |
| Franklin        | US 127              | 0.0-3.881              | 0.0-3.881     | 1990-1993              | 3                | 9,958          | 15,304       |
| Hardin          | US 62               | 10.8-14.56             | 10.8-14.56    | 1991-1992              | 3                | 5,001          | 7,000        |
| Hardin          | US 62               | 14.57-17.5             | 14.57-17.5    | 1991-1992              | 3                | 10,572         | 15,539       |
| Hardin          | KY 3005             | 5.926-8.674            | 5.926-8.674   | 1995-1996              | 3                | 7,380          | 11,600       |
| Jefferson       | US 31 E             | 0.0-4.325              | 0.0-4.325     | 1995-1998              | 1                | 18,453         | 22,244       |
| Jessamine       | US 27               | 1.179-5.803            | 1.179-6.008   | 1995-1997              | 2                | 15,985         | 20,869       |
| Johnson         | US 23               | 4.322-8.7              | 2.508-7.095   | 1993-1996              | 3                | 11,297         | 12,164       |
| Johnson         | US 23               | 0.0-4.321              | 0.0-2.507     | 1992-1996              | 3                | 9,233          | 13,000       |
| Knox            | US 25 E             | 0.0-5.1                | 0.0-4.9       | 1991-1995              | 3                | 6,475          | 9,198        |
| Logan           | US 68               | 19.139-22.159          | 19.139-22.091 | 1991-1995              | 3                | 5,740          | 8,133        |
| Logan           | US 68               | 22.16-26.567           | 22.092-26.733 | 1992-1996              | 3                | 5,538          | 8,084        |
| Pike            | US 23               | 16.267-21.56           | 16.267-20.295 | 1989-1992              | 3                | 8,300          | 12,150       |
| Pike            | US 119              | 12.0-15.0              | 11.965-14.86  | 1993-1997              | 3                | 6,430          | 7,530        |
| Trigg           | US 68               | 20.506-24.266          | 20.74-24.5    | 1993-1994              | 3                | 5,821          | 8,559        |
| Trigg           | US 68               | 24.267-26.266          |               | 1995-1997              | 2                | 4,882          | 5,191        |
| Warren          | US 68               | 0.0-5.0                | 0.0-5.0       | 1993-1996              | 3                | 5,734          | 6,544        |

Table 1. Summary of Highway Construction Locations (continued)

|               |                |               |               |              |                  | Average | Daily |
|---------------|----------------|---------------|---------------|--------------|------------------|---------|-------|
|               |                | Milepoint Ra  | _             | Construction | Time Before/     | Traf    |       |
| County        | Route          | Before        | After         | Period       | After Data (Yrs) | Before  | After |
| Upgrading Two | o-Lane Roadway |               |               |              |                  |         |       |
| Bath          | KY 11          | 11-12.749     | 11-12.783     | 1993-1994    | 3                | 1,100   | 1,560 |
| Boone         | KY 338         | 4.613-7.961   | 4.613-7.961   | 1995-1997    | 2                | 1,680   | 1,850 |
| Boyle         | KY 34          | 16.117-17.274 | 16.117-17.77  | 1991-1992    | 3                | 6,412   | 6,618 |
| Bracken       | KY 19          | 10.9-12.3     | 10.9-12.3     | 1992-1993    | 3                | 846     | 1,170 |
| Bullitt       | US 31 E        | 0-3.1         | 0-3.1         | 1997-1998    | 1                | 6,645   | 6,852 |
| Casey         | US 127         | 0-3.452       | 0-3.452       | 1991-1993    | 3                | 2,220   | 2,582 |
| Casey         | US 127         | 6.266-7.478   | 6.266-7.478   | 1991-1992    | 3                | 2,037   | 3,375 |
| Casey         | US 127         | 9.957-11.898  | 9.957-11.898  | 1991-1993    | 3                | 2,770   | 3,600 |
| Fleming       | KY 11          | 0-2.8         | 0-2.6         | 1993-1994    | 3                | 1,120   | 1,310 |
| Franklin      | US 127         | 10.979-22.452 | 10.979-21.507 | 1992-1997    | 2                | 3,075   | 3,521 |
| Garrard       | KY 34          | 0-2.724       | 0-1.610       | 1991-1992    | 3                | 5,040   | 6,550 |
| Green         | US 68          | 16.3-18.411   | 16.3-18.411   | 1995-1997    | 2                | 5,150   | 6,960 |
| Green         | US 68          | 8.194-9.796   | 8.194-9.796   | 1991-1993    | 3                | 2,610   | 3,370 |
| Green         | US 68          | 9.796-11.344  | 9.796-11.344  | 1994-1995    | 3                | 2,610   | 3,370 |
| Harlan        | KY 38          | 4.733-6.658   | 4.233-6.658   | 1993-1994    | 3                | 6,680   | 8,610 |
| Harrison      | US 62          | 1.3-5.5       | 1.3-5.5       | 1992-1993    | 3                | 2,020   | 3,830 |
| Lincoln       | US 127         | 3.208-11.61   | 3.208-10.847  | 1991-1993    | 3                | 4,127   | 5,197 |
| Marion        | US 68          | 20.6-22.4     | 20.6-22.4     | 1993-1994    | 3                | 1,520   | 1,770 |
| Marion        | US 68          | 16.8-18.4     | 16.8-18.4     | 1992-1993    | 3                | 1,520   | 1,770 |
| Owen          | US 127         | 0-3.4         | 0-3.4         | 1996-1998    | 1                | 2,500   | 2,680 |
| Rowan         | KY 801         | 11.671-14.768 | 11.6-14.583   | 1995-1997    | 2                | 1,151   | 2,868 |
| Russell       | US 127         | 19.967-26.998 | 19.8-26.927   | 1993-1994    | 3                | 2,860   | 3,133 |
| Taylor        | US 68          | 0-3.475       | 0-3.475       | 1995-1997    | 2                | 6,101   | 7,242 |
| Washington    | US 150         | 12.738-19.797 | 12.738-19.797 | 1995-1997    | 2                | 1,955   | 2,204 |

Table 2. Before and After Crash Data

|              |             | Milepoir      | nt Range      | Average Dail | y Traffic | 100MV  | /M *    | Before/After | Total Cr | ashes | Rate(/100 | OMVM) | Percent   |
|--------------|-------------|---------------|---------------|--------------|-----------|--------|---------|--------------|----------|-------|-----------|-------|-----------|
| County       | Route       | Before        | After         | Before       | After     | Before | After   | Time (yrs)   | Before   | After | Before    | After | Reduction |
| Converting   | from two to | o four lanes  |               |              |           |        |         |              |          |       |           |       |           |
| Anderson     | US 127 B    | 0.0-6.831     | 0.0-6.656     | 8,838        | 14,041    | 0.6611 | 1.0234  | 3            | 136      | 86    | 206       | 84    | 59        |
| Anderson     | US 127      | 9.161-11.789  | 8.9-11.12     | 6,410        | 5,790     | 0.1845 | 0.1407  | 3            | 18       | 18    | 98        | 128   | -31       |
| Bell         | US 25 E     | 14.481-19.473 | 14.481-18.711 | 7,540        | 9,500     | 0.4122 | 0.4400  | 3            | 42       | 34    | 102       | 77    | 24        |
| Boyle        | US 127      | 0.0-2.972     | 0.314-3.443   | 9,369        | 12,546    | 0.3049 | 0.4299  | 3            | 163      | 184   | 535       | 428   | 20        |
| Bullitt      | US 31 E     | 3.2-5.465     | 3.2-5.185     | 10,200       | 13,580    | 0.2530 | 0.2952  | 3            | 165      | 47    | 652       | 159   | 76        |
| Christian    | US 68       | 7.3-8.75      | 7.3-8.75      | 5,900        | 6,900     | 0.0625 | 0.0730  | 2            | 12       | 12    | 192       | 164   | 14        |
| Daviess      | US 60       | 19.332-23.558 | 19.326-23.842 | 10,219       | 15,539    | 0.3153 | 0.5123  | 2            | 41       | 32    | 130       | 62    | 52        |
| Floyd        | US 23       | 21.297-23.801 | 20.445-21.878 | 10,200       | 12,600    | 0.2797 | 0.1977  | 3            | 79       | 38    | 282       | 192   | 32        |
| Floyd        | US 23       | 18.153-21.296 | 17.489-20.444 | 14,500       | 15,700    | 0.4990 | 0.5080  | 3            | 81       | 35    | 162       | 69    | 58        |
| ranklin      | US 127      | 0.0-3.881     | 0.0-3.881     | 9,958        | 15,304    | 0.4232 | 0.6504  | 3            | 200      | 76    | 473       | 117   | 75        |
| Hardin       | US 62       | 10.8-14.56    | 10.8-14.56    | 5,001        | 7,000     | 0.2059 | 0.2882  | 3            | 47       | 26    | 228       | 90    | 60        |
| Hardin       | US 62       | 14.57-17.5    | 14.57-17.5    | 10,572       | 15,539    | 0.3392 | 0.4985  | 3            | 122      | 126   | 360       | 253   | 30        |
| Hardin       | KY 3005     | 5.926-8.674   | 5.926-8.674   | 7,380        | 11,600    | 0.2221 | 0.3491  | 3            | 68       | 51    | 306       | 146   | 52        |
| lefferson    | US 31 E     | 0.0-4.325     | 0.0-4.325     | 18,453       | 22,244    | 0.2913 | 0.3511  | 1            | 60       | 17    | 206       | 48    | 76        |
| lessamine    | US 27       | 1.179-5.803   | 1.179-6.008   | 15,985       | 20,869    | 0.5396 | 0.7357  | 2            | 130      | 85    | 241       | 116   | 52        |
| lohnson      | US 23       | 4.322-8.7     | 2.508-7.095   | 11,297       | 12,164    | 0.5416 | 0.6110  | 3            | 96       | 25    | 177       | 41    | 77        |
| Johnson      | US 23       | 0.0-4.321     | 0.0-2.507     | 9,233        | 13,000    | 0.4369 | 0.3569  | 3            | 77       | 13    | 176       | 36    | 79        |
| <b>C</b> nox | US 25 E     | 0.0-5.1       | 0.0-4.9       | 6,475        | 9,198     | 0.3616 | 0.4935  | 3            | 79       | 41    | 218       | 83    | 62        |
| ogan_        | US 68       | 19.139-22.159 | 19.139-22.091 | 5,740        | 8,133     | 0.1898 | 0.2629  | 3            | 39       | 44    | 205       | 167   | 19        |
| ₋ogan        | US 68       | 22.16-26.567  | 22.092-26.733 | 5,538        | 8,084     | 0.2672 | 0.4108  | 3            | 36       | 31    | 135       | 75    | 44        |
| Pike         | US 23       | 16.267-21.56  | 16.267-20.295 | 8,300        | 12,150    | 0.4811 | 0.5359  | 3            | 180      | 35    | 374       | 65    | 83        |
| Pike         | US 119      | 12.0-15.0     | 11.965-14.86  | 6,430        | 7,530     | 0.2112 | 0.2387  | 3            | 72       | 11    | 341       | 46    | 86        |
| rigg         | US 68       | 20.506-24.266 | 20.74-24.5    | 5,821        | 8,559     | 0.2397 | 0.3524  | 3            | 67       | 51    | 280       | 145   | 48        |
| rigg         | US 68       | 24.267-26.266 | 24.501-26.5   | 4,882        | 5,191     | 0.0712 | 0.0758  | 2            | 6        | 3     | 84        | 40    | 53        |
| Varren       | US 68       | 0.0-5.0       | 0.0-5.0       | 5,734        | 6,544     | 0.3139 | 0.3583  | 3            | 78       | 37    | 248       | 103   | 58        |
| AII          |             |               |               | 8,799        | 11,572    | 8.1074 | 10.1893 |              | 2094     | 1158  | 258       | 114   | 56        |

<sup>\* 100</sup> million vehicle miles traveled over milepoint range in before or after time period

Table 2. Before and After Crash Data (continued)

|            | Milepoint Range |               | Average Daily Traffic 100MVM * |        |       |        | Before/After Total Crashes |            |        | Rate(/100 | Percent |       |           |
|------------|-----------------|---------------|--------------------------------|--------|-------|--------|----------------------------|------------|--------|-----------|---------|-------|-----------|
| County     | Route           | Before        | After                          | Before | After | Before | After                      | Time (yrs) | Before | After     | Before  | After | Reduction |
| Jpgrading  | two-lane ro     | adway         |                                |        |       |        |                            |            |        |           |         |       |           |
| Bath       | KY 11           | 11-12.749     | 11-12.783                      | 1,100  | 1,560 | 0.0211 | 0.0305                     | 3          | 10     | 3         | 475     | 98    | 79        |
| Boone      | KY 338          | 4.613-7.961   | 4.613-7.961                    | 1,680  | 1,850 | 0.0411 | 0.0452                     | 2          | 8      | 16        | 195     | 354   | -82       |
| Boyle      | KY 34           | 16.117-17.274 | 16.117-17.77                   | 6,412  | 6,618 | 0.0812 | 0.1198                     | 3          | 16     | 11        | 197     | 92    | 53        |
| Bracken    | KY 19           | 10.9-12.3     | 10.9-12.3                      | 846    | 1,170 | 0.0130 | 0.0179                     | 3          | 4      | 6         | 308     | 335   | -8        |
| Bullitt    | US 31 E         | 0-3.1         | 0-3.1                          | 6,645  | 6,852 | 0.0752 | 0.0775                     | 1          | 22     | 9         | 293     | 116   | 60        |
| Casey      | US 127          | 0-3.452       | 0-3.452                        | 2,220  | 2,582 | 0.0839 | 0.0976                     | 3          | 22     | 7         | 262     | 72    | 73        |
| Casey      | US 127          | 6.266-7.478   | 6.266-7.478                    | 2,037  | 3,375 | 0.0270 | 0.0448                     | 3          | 10     | 1         | 370     | 22    | 94        |
| Casey      | US 127          | 9.957-11.898  | 9.957-11.898                   | 2,770  | 3,600 | 0.0589 | 0.0765                     | 3          | 8      | 0         | 136     | 0     | 100       |
| Fleming    | KY 11           | 0-2.8         | 0-2.6                          | 1,120  | 1,310 | 0.0343 | 0.0373                     | 3          | 25     | 26        | 728     | 697   | 4         |
| Franklin   | US 127          | 10.979-22.452 | 10.979-21.507                  | 3,075  | 3,521 | 0.2575 | 0.2706                     | 2          | 83     | 39        | 322     | 144   | 55        |
| Garrard    | KY 34           | 0-2.724       | 0-1.610                        | 5,040  | 6,550 | 0.1503 | 0.1155                     | 3          | 27     | 2         | 180     | 17    | 90        |
| Green      | US 68           | 16.3-18.411   | 16.3-18.411                    | 5,150  | 6,960 | 0.0794 | 0.1073                     | 2          | 17     | 10        | 214     | 93    | 56        |
| Green      | US 68           | 8.194-9.796   | 8.194-9.796                    | 2,610  | 3,370 | 0.0458 | 0.0591                     | 3          | 8      | 9         | 175     | 152   | 13        |
| Green      | US 68           | 9.796-11.344  | 9.796-11.344                   | 2,610  | 3,370 | 0.0442 | 0.0571                     | 3          | 16     | 8         | 362     | 140   | 61        |
| Harlan     | KY 38           | 4.733-6.658   | 4.233-6.658                    | 6,680  | 8,610 | 0.1408 | 0.2286                     | 3          | 41     | 55        | 291     | 241   | 17        |
| Harrison   | US 62           | 1.3-5.5       | 1.3-5.5                        | 2,020  | 3,830 | 0.0929 | 0.1761                     | 3          | 40     | 12        | 431     | 68    | 84        |
| Lincoln    | US 127          | 3.208-11.61   | 3.208-10.847                   | 4,127  | 5,197 | 0.3797 | 0.4347                     | 3          | 106    | 40        | 279     | 92    | 67        |
| Marion     | US 68           | 20.6-22.4     | 20.6-22.4                      | 1,520  | 1,770 | 0.0300 | 0.0349                     | 3          | 4      | 4         | 134     | 115   | 14        |
| Marion     | US 68           | 16.8-18.4     | 16.8-18.4                      | 1,520  | 1,770 | 0.0266 | 0.0310                     | 3          | 5      | 7         | 188     | 226   | -20       |
| Owen       | US 127          | 0-3.4         | 0-3.4                          | 2,500  | 2,680 | 0.0310 | 0.0333                     | 1          | 1      | 0         | 32      | 0     | 100       |
| Rowan      | KY 801          | 11.671-14.768 | 11.6-14.583                    | 1,151  | 2,868 | 0.0260 | 0.0625                     | 2          | 8      | 17        | 307     | 272   | 11        |
| Russell    | US 127          | 19.967-26.998 | 19.8-26.927                    | 2,860  | 3,133 | 0.2202 | 0.2445                     | 3          | 42     | 25        | 191     | 102   | 46        |
| Taylor     | US 68           | 0-3.475       | 0-3.475                        | 6,101  | 7,242 | 0.1548 | 0.1837                     | 2          | 21     | 13        | 136     | 71    | 48        |
| Washington | US 150          | 12.738-19.797 | 12.738-19.797                  | 1,955  | 2,204 | 0.1007 | 0.1136                     | 2          | 10     | 10        | 99      | 88    | 11        |
| All        |                 |               |                                | 3,073  | 3,833 | 2.2157 | 2.6996                     |            | 554    | 330       | 250     | 122   | 51        |

<sup>\* 100</sup> million vehicle miles traveled over milepoint range in before or after time period

Table 3. Before and After Injury and Fatal Crash Data

|              | Milepoint Range |              | Average Dail     | Average Daily Traffic 100MVM * |        | /M *   | Before/After | Fatal/Injury | ury Crashes Rate(/ |       | ate(/100MVM) |       |           |
|--------------|-----------------|--------------|------------------|--------------------------------|--------|--------|--------------|--------------|--------------------|-------|--------------|-------|-----------|
| County       | Route           | Before       | After            | Before                         | After  | Before | After        | Time (yrs)   | Before             | After | Before       | After | Reduction |
| Converting   | from two t      | o four lanes |                  |                                |        |        |              |              |                    |       |              |       |           |
| Anderson     | US 127 B        | 0.0-6.831    | 0.0-6.656        | 8,838                          | 14,041 | 0.6611 | 1.0234       | 3            | 50                 | 38    | 76           | 37    | 51        |
| Anderson     | US 127          | 9.161-11.789 | 9 8.9-11.12      | 6,410                          | 5,790  | 0.1845 | 0.1407       | 3            | 5                  | 8     | 27           | 57    | -110      |
| Bell         | US 25 E         | 14.481-19.47 | 73 14.481-18.711 | 7,540                          | 9,500  | 0.4122 | 0.4400       | 3            | 15                 | 13    | 36           | 30    | 19        |
| Boyle        | US 127          | 0.0-2.972    | 0.314-3.443      | 9,369                          | 12,546 | 0.3049 | 0.4299       | 3            | 51                 | 54    | 167          | 126   | 25        |
| Bullitt      | US 31 E         | 3.2-5.465    | 3.2-5.185        | 10,200                         | 13,580 | 0.2530 | 0.2952       | 3            | 48                 | 15    | 190          | 51    | 73        |
| Christian    | US 68           | 7.3-8.75     | 7.3-8.75         | 5,900                          | 6,900  | 0.0625 | 0.0730       | 2            | 4                  | 6     | 64           | 82    | -28       |
| Daviess      | US 60           | 19.332-23.55 | 58 19.326-23.842 | 10,219                         | 15,539 | 0.3153 | 0.5123       | 2            | 16                 | 15    | 51           | 29    | 42        |
| Floyd        | US 23           | 21.297-23.80 | 01 20.445-21.878 | 10,200                         | 12,600 | 0.2797 | 0.1977       | 3            | 41                 | 24    | 147          | 121   | 17        |
| Floyd        | US 23           | 18.153-21.29 | 96 17.489-20.444 | 14,500                         | 15,700 | 0.4990 | 0.5080       | 3            | 32                 | 22    | 64           | 43    | 32        |
| ranklin      | US 127          | 0.0-3.881    | 0.0-3.881        | 9,958                          | 15,304 | 0.4232 | 0.6504       | 3            | 64                 | 33    | 151          | 51    | 66        |
| Hardin       | US 62           | 10.8-14.56   | 10.8-14.56       | 5,001                          | 7,000  | 0.2059 | 0.2882       | 3            | 19                 | 8     | 92           | 28    | 70        |
| Hardin       | US 62           | 14.57-17.5   | 14.57-17.5       | 10,572                         | 15,539 | 0.3392 | 0.4985       | 3            | 31                 | 39    | 91           | 78    | 14        |
| Hardin       | KY 3005         | 5.926-8.674  | 5.926-8.674      | 7,380                          | 11,600 | 0.2221 | 0.3491       | 3            | 18                 | 9     | 81           | 26    | 68        |
| lefferson    | US 31 E         | 0.0-4.325    | 0.0-4.325        | 18,453                         | 22,244 | 0.2913 | 0.3511       | 1            | 20                 | 5     | 69           | 14    | 79        |
| lessamine    | US 27           | 1.179-5.803  | 1.179-6.008      | 15,985                         | 20,869 | 0.5396 | 0.7357       | 2            | 49                 | 19    | 91           | 26    | 72        |
| lohnson      | US 23           | 4.322-8.7    | 2.508-7.095      | 11,297                         | 12,164 | 0.5416 | 0.6110       | 3            | 40                 | 14    | 74           | 23    | 69        |
| lohnson      | US 23           | 0.0-4.321    | 0.0-2.507        | 9,233                          | 13,000 | 0.4369 | 0.3569       | 3            | 41                 | 7     | 94           | 20    | 79        |
| <b>C</b> nox | US 25 E         | 0.0-5.1      | 0.0-4.9          | 6,475                          | 9,198  | 0.3616 | 0.4935       | 3            | 23                 | 15    | 64           | 30    | 52        |
| ₋ogan        | US 68           | 19.139-22.15 | 59 19.139-22.091 | 5,740                          | 8,133  | 0.1898 | 0.2629       | 3            | 10                 | 20    | 53           | 76    | -44       |
| ₋ogan        | US 68           | 22.16-26.567 | 7 22.092-26.733  | 5,538                          | 8,084  | 0.2672 | 0.4108       | 3            | 16                 | 5     | 60           | 12    | 80        |
| Pike         | US 23           | 16.267-21.56 | 6 16.267-20.295  | 8,300                          | 12,150 | 0.4811 | 0.5359       | 3            | 75                 | 21    | 156          | 39    | 75        |
| Pike         | US 119          | 12.0-15.0    | 11.965-14.86     | 6,430                          | 7,530  | 0.2112 | 0.2387       | 3            | 24                 | 8     | 114          | 34    | 71        |
| Γrigg        | US 68           | 20.506-24.26 | 66 20.74-24.5    | 5,821                          | 8,559  | 0.2397 | 0.3524       | 3            | 23                 | 20    | 96           | 57    | 41        |
| rigg         | US 68           | 24.267-26.26 | 66 24.501-26.5   | 4,882                          | 5,191  | 0.0712 | 0.0758       | 2            | 4                  | 3     | 56           | 40    | 29        |
| Varren       | US 68           | 0.0-5.0      | 0.0-5.0          | 5,734                          | 6,544  | 0.3139 | 0.3583       | 3            | 34                 | 9     | 108          | 25    | 77        |
| All          |                 |              |                  | 8,799                          | 11,572 | 8.1074 | 10.1893      |              | 753                | 430   | 93           | 42    | 55        |

<sup>\* 100</sup> million vehicle miles traveled over milepoint range in before or after time period

Table 3. Before and After Injury and Fatal Crash Data (continued)

|           | Milepoint Range |              | Average Daily Traffic 100MVM * |        |       | Before/After Fatal/Injury Crashes |        |            | Rate(/100 | MVM)  | Percent |       |           |
|-----------|-----------------|--------------|--------------------------------|--------|-------|-----------------------------------|--------|------------|-----------|-------|---------|-------|-----------|
| County    | Route           | Before       | After                          | Before | After | Before                            | After  | Time (yrs) | Before    | After | Before  | After | Reduction |
| Jpgrading | two-lane ro     | oadway       |                                |        |       |                                   |        |            |           |       |         |       |           |
| Bath      | KY 11           | 11-12.749    | 11-12.783                      | 1,100  | 1,560 | 0.0211                            | 0.0305 | 3          | 6         | 1     | 285     | 33    | 88        |
| Boone     | KY 338          | 4.613-7.961  | 4.613-7.961                    | 1,680  | 1,850 | 0.0411                            | 0.0452 | 2          | 6         | 9     | 146     | 199   | -36       |
| Boyle     | KY 34           | 16.117-17.27 | 416.117-17.77                  | 6,412  | 6,618 | 0.0812                            | 0.1198 | 3          | 6         | 4     | 74      | 33    | 55        |
| Bracken   | KY 19           | 10.9-12.3    | 10.9-12.3                      | 846    | 1,170 | 0.0130                            | 0.0179 | 3          | 2         | 3     | 154     | 167   | -8        |
| Bullitt   | US 31 E         | 0-3.1        | 0-3.1                          | 6,645  | 6,852 | 0.0752                            | 0.0775 | 1          | 7         | 3     | 93      | 39    | 58        |
| Casey     | US 127          | 0-3.452      | 0-3.452                        | 2,220  | 2,582 | 0.0839                            | 0.0976 | 3          | 11        | 6     | 131     | 61    | 53        |
| Casey     | US 127          | 6.266-7.478  | 6.266-7.478                    | 2,037  | 3,375 | 0.0270                            | 0.0448 | 3          | 5         | 1     | 185     | 22    | 88        |
| Casey     | US 127          | 9.957-11.898 | 9.957-11.898                   | 2,770  | 3,600 | 0.0589                            | 0.0765 | 3          | 6         | 0     | 102     | 0     | 100       |
| Fleming   | KY 11           | 0-2.8        | 0-2.6                          | 1,120  | 1,310 | 0.0343                            | 0.0373 | 3          | 9         | 8     | 262     | 215   | 18        |
| Franklin  | US 127          | 10.979-22.45 | 52 10.979-21.507               | 3,075  | 3,521 | 0.2575                            | 0.2706 | 2          | 31        | 11    | 120     | 41    | 66        |
| Garrard   | KY 34           | 0-2.724      | 0-1.610                        | 5,040  | 6,550 | 0.1503                            | 0.1155 | 3          | 8         | 2     | 53      | 17    | 67        |
| Green     | US 68           | 16.3-18.411  | 16.3-18.411                    | 5,150  | 6,960 | 0.0794                            | 0.1073 | 2          | 6         | 4     | 76      | 37    | 51        |
| Green     | US 68           | 8.194-9.796  | 8.194-9.796                    | 2,610  | 3,370 | 0.0458                            | 0.0591 | 3          | 5         | 1     | 109     | 17    | 85        |
| Green     | US 68           | 9.796-11.344 | 9.796-11.344                   | 2,610  | 3,370 | 0.0442                            | 0.0571 | 3          | 5         | 4     | 113     | 70    | 38        |
| Harlan    | KY 38           | 4.733-6.658  | 4.233-6.658                    | 6,680  | 8,610 | 0.1408                            | 0.2286 | 3          | 19        | 24    | 135     | 105   | 22        |
| Harrison  | US 62           | 1.3-5.5      | 1.3-5.5                        | 2,020  | 3,830 | 0.0929                            | 0.1761 | 3          | 17        | 3     | 183     | 17    | 91        |
| Lincoln   | US 127          | 3.208-11.61  | 3.208-10.847                   | 4,127  | 5,197 | 0.3797                            | 0.4347 | 3          | 43        | 19    | 113     | 44    | 61        |
| Marion    | US 68           | 20.6-22.4    | 20.6-22.4                      | 1,520  | 1,770 | 0.0300                            | 0.0349 | 3          | 3         | 1     | 100     | 29    | 71        |
| Marion    | US 68           | 16.8-18.4    | 16.8-18.4                      | 1,520  | 1,770 | 0.0266                            | 0.0310 | 3          | 1         | 3     | 38      | 97    | -158      |
| Owen      | US 127          | 0-3.4        | 0-3.4                          | 2,500  | 2,680 | 0.0310                            | 0.0333 | 1          | 1         | 0     | 32      | 0     | 100       |
| Rowan     | KY 801          | 11.671-14.76 | 8811.6-14.583                  | 1,151  | 2,868 | 0.0260                            | 0.0625 | 2          | 5         | 6     | 192     | 96    | 50        |
| Russell   | US 127          | 19.967-26.99 | 8 19.8-26.927                  | 2,860  | 3,133 | 0.2202                            | 0.2445 | 3          | 16        | 8     | 73      | 33    | 55        |
| Taylor    | US 68           | 0-3.475      | 0-3.475                        | 6,101  | 7,242 | 0.1548                            | 0.1837 | 2          | 8         | 5     | 52      | 27    | 47        |
| Nashingto | n US 150        | 12.738-19.79 | 7 12.738-19.797                | 1,955  | 2,204 | 0.1007                            | 0.1136 | 2          | 5         | 3     | 50      | 26    | 47        |
| AII       |                 |              | ·                              | 3,073  | 3,833 | 2.2157                            | 2.6996 |            | 231       | 129   | 104     | 48    | 54        |

<sup>\* 100</sup> million vehicle miles traveled over milepoint range in before or after time period

Table 4. Detailed Analysis of Accident Charateristics

|                              |                                    |  | Rate (10 | O MVM)  | Percent   | Pero   | ent   | Percent   |
|------------------------------|------------------------------------|--|----------|---------|-----------|--------|-------|-----------|
| Construction Type            | Characteristic                     | Description                                      | Before   | After   | Reduction | Before | After | Reduction |
| Occupation from Torre to For |                                    |  |          |         |           |        |       |           |
| Converting from Two- to Fou  | Type of Crash                      | Other motor vehicle                              | 191      | 84      | 56        | 74     | 74    | 0         |
| Roadway                      | Type of Crash                      | Other motor verticle Other collision (not-fixed) | 4        | 2       | 56<br>54  | 2      | 2     | 0<br>-5   |
|                              |                                    | Fixed object                                     | 55       | 23      | 58        | 21     | 20    | -5<br>5   |
|                              |                                    | Non-collision                                    | 8        | 23<br>5 | 42        | 3      | 4     | -31       |
|                              |                                    | Non-collision                                    | 8        | 5       | 42        | 3      | 4     | -31       |
|                              | Directional Analysis               | Intersection                                     |          |         |           |        |       |           |
|                              | ·                                  | Angle  | 30       | 27      | 10        | 12     | 24    | -104      |
|                              |                                    | Rear-end   | 24       | 12      | 53        | 9      | 10    | -8        |
|                              |                                    | All  | 71       | 47      | 33        | 27     | 42    | -52       |
|                              |                                    | Non-intersection                                 |          |         |           |        |       |           |
|                              |                                    | Rear-end   | 58       | 16      | 72        | 23     | 15    | 36        |
|                              |                                    | Sideswipe  | 36       | 12      | 67        | 14     | 10    | 26        |
|                              |                                    | Fixed object                                     | 26       | 7       | 74        | 10     | 6     | 40        |
|                              |                                    | Ran off road                                     | 19       | 5       | 77        | 8      | 4     | 47        |
|                              | Light Condition                    | Darkness   | 71       | 33      | 53        | 27     | 29    | -7        |
|                              | Road Surface                       | Wet  | 75       | 23      | 70        | 29     | 20    | 31        |
|                              |                                    | Snow/ice/slush                                   | 9        | 3       | 61        | 3      | 3     | 11        |
|                              |                                    | Unsafe Speed                                     | 31       | 8       | 74        | 12     | 7     | 41        |
|                              | Human Contributing Factor          | Failed to yield                                  | 49       | 30      | 39        | 19     | 26    | -38       |
|                              | 3                                  | Following too closely                            | 19       | 6       | 71        | 7      | 5     | 34        |
|                              |                                    | Improper passing                                 | 8        | 1       | 90        | 3      | 1     | 76        |
|                              |                                    | Alcohol  | 14       | 4       | 74        | 5      | 3     | 40        |
|                              |                                    | Driver inattention                               | 75       | 38      | 49        | 29     | 34    | -16       |
|                              | Environmental Contributing Fac     | etor All   | 78       | 28      | 64        | 30     | 25    | 17        |
|                              | 21171101111011101 Contributing Fat | Animal action                                    | 11       | 10      | 11        | 4      | 9     | -100      |
|                              |                                    | View limited                                     | 9        | 5       | 50        | 4      | 4     | -14       |
|                              |                                    | Slippery surface                                 | 42       | 8       | 81        | 16     | 7     | 55        |
|                              |                                    | Waterpooling                                     | 7        | 2       | 78        | 3      | 1     | 40        |
|                              |                                    | vvaterpooling                                    | 7        | 2       | 78        | 3      | 1     | 40        |

Table 4. Detailed Analysis of Accident Charateristics (continued)

|                            |                                   |                             | Rate (10 | 0 MVM) | Percent   | Perc   | ent   | Percent   |
|----------------------------|-----------------------------------|-----------------------------|----------|--------|-----------|--------|-------|-----------|
| Construction Type          | Characteristic                    | Description                 | Before   | After  | Reduction | Before | After | Reduction |
|                            |                                   |                             |          |        |           |        |       |           |
| Upgrading Two-Lane Roadway | Type of Crash                     | Other motor vehicle         | 131      | 74     | 44        | 52     | 60    | -15       |
|                            |                                   | Other collision (not-fixed) | 7        | 1      | 85        | 3      | 1     | 69        |
|                            |                                   | Fixed object                | 96       | 38     | 60        | 38     | 31    | 18        |
|                            |                                   | Non-collision               | 16       | 9      | 43        | 6      | 8     | -17       |
|                            | Directional Analysis              | Intersection                |          |        |           |        |       |           |
|                            | •                                 | Angle                       | 16       | 15     | 4         | 6      | 12    | -97       |
|                            |                                   | Rear-end                    | 14       | 6      | 55        | 6      | 5     | 8         |
|                            |                                   | All                         | 49       | 29     | 41        | 19     | 24    | -21       |
|                            |                                   | Non-intersection            |          |        |           |        |       |           |
|                            |                                   | Rear-end                    | 32       | 17     | 46        | 13     | 14    | -10       |
|                            |                                   | Sideswipe                   | 31       | 18     | 42        | 12     | 15    | -19       |
|                            |                                   | Fixed object                | 57       | 15     | 74        | 23     | 12    | 47        |
|                            |                                   | Ran off road                | 28       | 11     | 60        | 11     | 9     | 17        |
|                            | Light Condition                   | Darkness                    | 96       | 41     | 57        | 38     | 34    | 13        |
|                            | Road Surface                      | Wet                         | 75       | 22     | 71        | 30     | 18    | 40        |
|                            |                                   | Snow/ice/slush              | 15       | 6      | 59        | 6      | 5     | 16        |
|                            | Human Contributing Factor         | Unsafe Speed                | 34       | 11     | 67        | 14     | 9     | 32        |
|                            |                                   | Failed to yield             | 38       | 19     | 51        | 15     | 15    | 0         |
|                            |                                   | Following too closely       | 11       | 5      | 52        | 4      | 4     | 2         |
|                            |                                   | Improper passing            | 9        | 4      | 48        | 3      | 4     | -6        |
|                            |                                   | Alcohol                     | 18       | 8      | 57        | 7      | 6     | 12        |
|                            |                                   | Driver inattention          | 70       | 34     | 51        | 28     | 28    | -1        |
|                            | Environmental Contributing Factor | All                         | 88       | 37     | 58        | 35     | 30    | 14        |
|                            | •                                 | Animal action               | 14       | 16     | -16       | 5      | 13    | -135      |
|                            |                                   | View limited                | 8        | 4      | 47        | 3      | 3     | -6        |
|                            |                                   | Slippery surface            | 43       | 12     | 72        | 17     | 10    | 44        |
|                            |                                   | Waterpooling                | 2        | 1      | 52        | 1      | 1     | 0         |